

10/540226

3/PRTS

JC17 Rec'd PCT/PTO 21 JUN 2005
[10537/297]

PROCESS FOR THE PRODUCTION OF HEAT EXCHANGER TUBES CONSISTING
OF HALF-TUBES OR TUBES, FOR RECUPERATIVE WASTE GAS HEAT
EXCHANGERS

The present invention relates to a process for the production of half-tubes or tubes of a metallic, high-temperature-resistant material with a plurality of openings passing through their surface, for the fabrication of heat exchanger tubes for recuperative waste gas heat exchangers, as well as half-tubes/tubes produced by this process.

As is known, the recuperative waste gas heat exchangers used in gas turbine plants comprise, in addition to a heat exchanger housing, basically a distributor tube for feeding the "cold" air conveyed from a compressor into a so-called cross-counterflow matrix through which hot turbine waste gas flows, and a collecting tube for passing the now heated-up "hot" compressor air to a suitable consumer, for example the combustion chamber of the gas turbine plant. For the sake of simplicity the distributor tube as well as the collecting tube will hereinafter also be referred to as heat exchanger tube.

The feeding of the air from the distributor tube into the cross-counterflow matrix and the discharge of the air from the cross-counterflow matrix into the collecting tube is effected by a plurality of openings made in the surface of the heat exchanger tubes.

The cross-counterflow matrix comprises in turn a plurality of elliptical lancets or small tubes assembled to form a tubular bundle. The tubular bundle is arranged laterally and protruding in a U-shaped manner on the heat exchanger tubes arranged in parallel, the ends of each small tube of the tubular bundle corresponding in each case to an opening made

in the surface of the heat exchanger tubes. In order to be able to achieve the desired throughput, a plurality of lancets and accordingly a plurality of openings/holes are necessary in the surface of the heat exchanger tubes.

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The heat exchanger tubes consisting of a high-temperature-resistant material have up to now been assembled from forged half-tubes. The joining of two half-tubes to form a heat exchanger tube is effected by welding, and the attachment of 10 the lancets to the heat exchanger tubes is effected by means of high-temperature soldering.

According to a typical embodiment of a half-tube of length 500 mm and radius 62.5 mm, rows of holes each comprising 184 15 openings are provided on 19 circumferential positions, so that per half-tube a total of 3,496 openings are formed in the surface. For the production of the heat exchanger tubes of a recuperative waste gas heat exchanger from half-tubes, $4 \times 3,496 = 13,984$ holes/openings are therefore necessary in the 20 surface of the half-tubes.

The formation of such a large number of openings in the surface of the forged half-tubes proves to be extremely cost-intensive and time-consuming.

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The formation of the openings in the surface of the half-tubes has up to now therefore been achieved by spark erosion (EDM = electrodischarge machining). EDM is a known method for producing holes or other openings in metals. The principle of 30 the method, namely the thermal abrasion of small volumes by the high power density of a locally penetrating arc in the liquid dielectric acting on the anode (workpiece), involves a melting of the material in microscopic dimensions.

Apart from the high cost the EDM process has a further disadvantage. On account of the process-dependent procedure involved in the forming of the openings in the surface of the heat exchanger tubes re-solidified layers, the so-called 5 recast layers, are formed in the region of the perforation walls on the workpieces. These layers have to be removed before the high-temperature soldering to be carried out subsequently for soldering the lancets into the half-tubes, which proves to be a disadvantage and is complicated. The 10 narrow soldering gaps and small tolerances (± 0.05 mm) required for the high-temperature soldering often cannot be achieved with existing recast layers for economic reasons (a slow fine processing stage is necessary).

15 Electrochemical processing (ECM = electrochemical machining) is another option for forming the openings in the surface of the half-tubes. This method is costly however in terms of installation and tooling, and has capital-intensive equipment costs.

20 Also, the electrolyte in this process is typically an oxidizing agent, for example sodium nitrate or sodium chloride, which constitutes a health and security risk, and the by-products of the process are classified as toxic waste.

25 To summarize, this means that the formation of the openings in the surface of the forged half-tubes is a high-risk operation in terms of technology, time and cost in the production of the overall recuperative waste gas heat exchanger.

30 The object of the invention is to remedy this situation by means of a process for the production of such half-tubes or tubes of a metallic, high-temperature-resistant material with a plurality of openings passing through their surface, without 35 the disadvantages of the processes employed up to now.

This object is achieved according to the invention in that the half-tubes or tubes are produced as high-precision casting parts by employing a precision casting process.

5 Such a precision casting process has the advantage that it combines a high reproducibility with consistently high quality and low production costs.

10 In order to avoid reactions between the melt and ambient gases such as oxygen, nitrogen or hydrogen, at least the casting of the melt in the mold shell is carried out in the absence of reactive gases, in particular *in vacuo*, in an inert gas atmosphere or the like.

15 In order that also narrow cross-sections and fine contours can "run out" cleanly, the casting of the melt in hot mold shells is carried out *in vacuo* or under an excess pressure of inert gas.

20 A nickel-based alloy, in particular IN 625, is preferably used as high-temperature-resistant material for the precision casting process.

25 According to a preferred embodiment of the half-tubes or tubes produced according to the process, the openings passing through the surface have an elliptical shape. The radius of the half-tubes/tubes is 62.5 or 37.5 mm, and the length of the half-tubes is 500 mm or 750-900 mm.

30 The use according to the invention of a precision casting process known *per se* for the production of heat-exchanger tubes from half-tubes or tubes permits for the first time an inexpensive, quick and qualitatively high-grade production of
35 such tube components.

The invention is described in more detail hereinafter with the aid of an example of implementation illustrated more or less diagrammatically in the drawings, in which:

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Fig. 1 shows the basic structure of a recuperative waste gas heat exchanger,

10 Fig. 2 is a detailed view of a heat-exchanger tube, and

Fig. 3 shows the assembly of the heat-exchanger tube according to Fig. 2 from half-tubes.

15 A recuperative waste gas heat exchanger of a gas turbine plant (not shown here), identified overall in Fig. 1 by the reference numeral 10, essentially comprises a distributor tube 12, a collecting tube 14 arranged parallel thereto, as well as a cross-counterflow matrix 16 protruding laterally thereto in a U-shape. For the sake of simplicity the distributor tube 12
20 and collecting tube 14 are identified hereinafter as heat exchanger tubes.

25 From the cross-sectional view of the cross-counterflow matrix 16 shown in the bottom left-hand corner of Fig. 1, it can be seen that the cross-counterflow matrix 16 comprises a plurality of elliptical small tubes or lancets 18. The lancets 18 are in each case secured to the distributor tube 12 and collecting tube 14. They correspond to the openings/holes 22, not visible in this representation, made for this purpose
30 in the surface of the distributor tube 12 and the collecting tube 14 (cf. Fig. 2).

The mode of operation of the recuperative waste gas heat exchanger described hereinbefore is as follows:

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Cold compressed air is fed from a compressor in the direction of the arrow D to the distributor tube 12. The cold compressed air flows from the distributor tube 12 through the openings/holes made in the surface into the laterally protruding, U-shaped cross-counterflow matrix 16. The cold compressor air is heated up by the circulating flow of the hot turbine waste gas H through the cross-counterflow matrix 16. After flowing through the cross-counterflow matrix 16 and entering the collecting tube 14, the now hot air is fed in the direction of the arrow D' to a suitable consumer, e.g. the combustion chamber.

Fig. 2 shows on an enlarged scale a detailed view of a perforated heat exchanger tube 12/14 of the recuperative waste gas heat exchanger 10. The heat exchanger tube 12/14 has a plurality of openings 22 passing through its surface 20. The openings 22 are elliptical in shape. Of this large number of openings 22 in the surface 20, for the sake of clarity only a few of the openings 22 passing through the surface 20 of the heat exchanger tube 12/14 are shown here. For the sake of completeness it may however be mentioned that 184 rows of holes, i.e. 3,496 openings 22, are provided per half-tube of dimensions 500 mm in length and radius 62.5 mm. A total of $2 \times 3,496 = 6,992$ openings 22 passing through the surface 20 are thus produced per heat exchanger tube 12/14.

In this example the heat exchanger tube 12/14 is, as shown in Fig. 3, assembled from a first half-tube 24 and a second half-tube 26. The joining of the two half-tubes 24, 26 is carried out by fusion welding, and the installation of the lancets is performed in a known manner by means of high temperature soldering.

The production of the half-tubes 24, 26 by means of a precision casting method known *per se* will now be described in

detail, in which the process steps -- with the exception of the assembly of the half-tubes -- apply in the same way also to the production of a tube, i.e. a complete tube.

5 To this end, in a first process step a fine-structured, dimensionally accurate model of the half-tubes 24, 26 destroyable by heating, including the openings 22 passing through the surface 20, is first of all produced. Wax is used as the model material for this purpose.

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The wax model including the wax gate system receives a mold shell by immersion in ceramic coating compositions followed by sanding with casting shell ceramics material. In order to ensure the stability of the mold shell, the automated process
15 of immersion followed by sanding is repeated several times.

After the model has been melted, preferably in an autoclave using superheated steam, the single-piece mold shells that are thereby formed are fired, thereby acquiring their fire
20 resistance. This is followed by the casting of the melt into hot mold shells by employing a vacuum or under excess pressure of an inert gas.

In this way it is ensured that also the narrow cross-sections
25 between two openings 22 in the surface 20 of a half-tube 24, 26 "run out" cleanly. The melting and casting of the half-tube material is carried out under a high vacuum. A nickel-based alloy with the standard reference IN 625 (INCONEL) is used as material.

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The cast half-tubes 24, 26 should then be cleaned and trimmed, in which connection the sprues should also be removed. For the fabrication of the half-tubes 24, 26 a post-treatment of the openings 22 passing through the surface 20 should if
35 necessary also be carried out in a last workstage by blasting

with erosive abrasives or by a "facing operation" by means of EDM (electrodischarge machining). Because of the high quality and tight tolerances of the precision casting method that is used, only a short processing time is required for this
5 purpose. The recast layers hitherto formed by producing the openings by means of EDM can be greatly minimized and therefore disregarded, since they are negligibly thin and small as a result of the short processing time.

10 The assembly of two such half-tubes 24, 26 to form a heat exchanger tube 12/14 is carried out by a fusion welding process, which is likewise known. The introduction of the lancets made of IN 625 into the elliptical perforations is carried out by a highly automated assembly and soldering
15 operation with soldering paste by means of vacuum high-temperature soldering.